Correction to "Mode Classification of a Triangular Ferrite Post for Y-Circulator Operation"

Y. AKAIWA

In the above paper,[1] the following corrections should be made.

Equation (6) should read as

$$E_x = \frac{\beta}{\omega\epsilon} H_y. \tag{6}$$

Equation (7) should read as

$$E_y = \frac{-\beta}{\omega\epsilon} H_x. \tag{7}$$

Equation (22) should read as

$$\frac{\Delta\omega^{\pm}}{\omega} = \pm \frac{\sqrt{3}}{2\pi} \frac{\kappa}{\mu}. \tag{22}$$

In the last phrase, the sentence, *The preceding result indicates a bandwidth of about two times compared with that of cylindrical ferrite post lowest mode*, should be deleted.

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The author is with the Central Research Laboratories, Nippon Electric Company, Ltd., Kawasaki, Japan.

[1] Y. Akaiwa, "Mode classification of a triangular ferrite post for Y-circulator operation," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-25, pp. 59–61, Jan. 1977.

Correction to "Operation Modes of a Waveguide Y Circulator"

Y. AKAIWA

In the above paper,[1] the following corrections should be made.

Equation (23) should read as

$$H_z = -\frac{\chi^2}{j\omega\mu} \psi. \tag{23}$$

Equation (34) should read as

$$E_x = \frac{k_l}{\omega\epsilon} H_y. \tag{34}$$

Equation (35) should read as

$$E_y = -\frac{k_l}{\omega\epsilon} H_x. \tag{35}$$

Fig. 14 should be drawn as Fig. 3 in the paper[2] published recently.

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The author is with the Central Research Laboratories, Nippon Electric Company, Ltd., Kawasaki, Japan.

[1] Y. Akaiwa, "Operation modes of a waveguide Y circulator," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-22, pp. 954–960, Nov. 1974.

[2] J. Helszajn, D. S. James, and W. T. Nisbet, "Circulators using planar triangular resonators," *IEEE Trans. Microwave Theory Tech.*, vol. MTT-27, pp. 188–193, Feb. 1979.

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